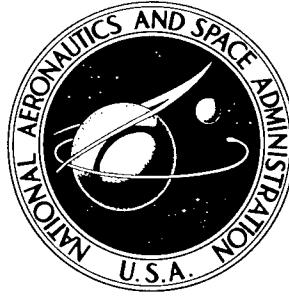


61893

NASA TECHNICAL NOTE



NASA TN D-3040

NASA TN D-3040

PROPERTY OF:

**DISTRIBUTION STATEMENT A**  
Approved for Public Release  
Distribution Unlimited

**VAPOR-DEPOSITED THIN GOLD FILMS  
AS LUBRICANTS IN VACUUM ( $10^{-11}$  mm Hg)**

*by Talivaldis Spalvins and Donald H. Buckley*

*Lewis Research Center  
Cleveland, Ohio*

20020412 115

NASA TN D-3040

VAPOR-DEPOSITED THIN GOLD FILMS AS LUBRICANTS IN VACUUM

( $10^{-11}$  mm Hg)

By Talivaldis Spalvins and Donald H. Buckley

Lewis Research Center  
Cleveland, Ohio

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

---

For sale by the Clearinghouse for Federal Scientific and Technical Information  
Springfield, Virginia 22151 - Price \$1.00

# VAPOR-DEPOSITED THIN GOLD FILMS AS LUBRICANTS IN VACUUM ( $10^{-11}$ mm Hg)

by Talivaldis Spalvins and Donald H. Buckley

Lewis Research Center

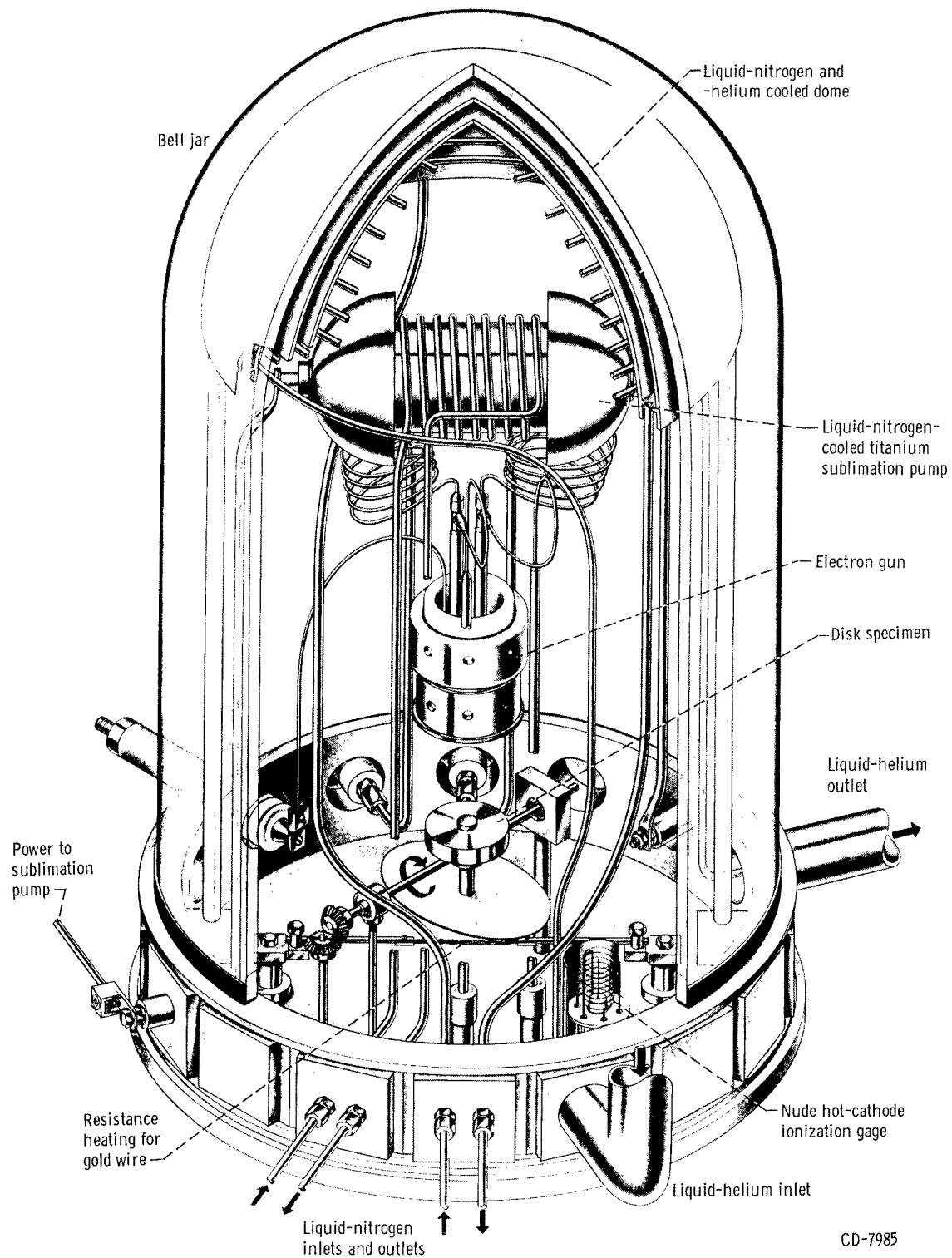
## SUMMARY

start  
Thin gold films were vapor-deposited on nickel, nickel-chromium, and nickel rhenium surfaces to be used for lubrication purposes. The durability of the film was determined by friction characteristics. Durability and strong bonding (adhesion) between the film and the substrate are essential when thin films are used as lubricants. Two methods of substrate preparation for vapor deposition were investigated: (1) mechanical polishing and (2) electron bombardment. Friction experiments were conducted with a hemispherical niobium rider sliding on the deposited gold film on a rotating disk. Results of this investigation indicated that the film endurance life during friction experiments was increased when the substrate was electron bombarded and thermally etched prior to vapor deposition on the etched surface at an elevated temperature of 800° F. A diffusion-type interface was believed to be formed between the film and the substrate. Re- p 12 end

## INTRODUCTION

Thin, soft metal films may be used as lubricants in outer space for rotating or sliding components to reduce the coefficient of friction and to eliminate complete seizure of the moving parts. Previous experiments have shown that thin metal films deposited conventionally have very limited operational lives because of the weak adhesion of film to substrate (ref. 1). This weakly bonded film, when brought into sliding contact with another surface, is subject to easy rupturing, and thus its use as a lubricant is limited.

References 2 to 4 describe in great detail the deposition parameters for thin-film preparation, mostly on glass substrates, with special emphasis on the structural, mechanical, optical, and magnetic properties of the thin film. Less consideration has been given to thin films vapor-deposited on metal substrates. The objective of this investigation was to study these vapor-deposited thin films and to obtain strong bonding (adhesion) between film and substrate. Strong bonding is essential for film durability in lubrication.



CD-7985

Figure 1. - High-vacuum vapor-deposition apparatus.

Two factors were considered: (1) material selection and (2) preparation of the substrate material.

The substrate and the film materials were selected on the basis of solid-solubility principles (ref. 5) and thermal-expansion coefficients. If two materials are mutually soluble, diffusion and alloying take place at elevated temperatures, and, if the surface is atomically clean, vacuum deposition can then result in adherent films (ref. 6).

Adhesion of a vapor-deposited metal film to a substrate depends on the type and structure of the interfacial region and the nature of the bonding forces across this region (ref. 6). Hence, surface cleaning was investigated in order to achieve strong bonding (adhesion) between the substrate and the film.

The friction characteristics of vapor-deposited 1800-Å gold films on nickel, nickel - 10 percent-chromium, and nickel - 5-percent-rhenium substrates were determined under ultra-high-vacuum conditions ( $10^{-11}$  mm Hg). The experiments were conducted with a hemispherical rider of niobium (which is slightly miscible with gold or nickel) sliding on the thin film on a disk. The rider was run at a load of 250 grams, a speed of 5 feet per minute, and ambient temperature.

## APPARATUS

### Vacuum Vapor-Deposition Apparatus

The vacuum vapor-deposition apparatus in figure 1 basically consists of a commercial evaporator unit with an 18-inch-diameter by 30-inch-high bell jar. A number of modifications were incorporated inside the bell jar for proper specimen mounting, inversion, electron bombardment, vapor deposition, and pumpdown to low pressures.

The  $2\frac{1}{2}$ -inch-diameter disk specimen is mounted on a stainless-steel specimen holder through which a circular rod is inserted for support and inversion. This inversion gives a proper positioning of the disk for electron bombardment and vapor deposition.

The specimen-mounting assembly has a fixed adjustment; that is, when the disk is positioned for electron bombardment, it is always 3 inches from the electron gun, and when the disk is inverted for vapor deposition, it is 3.5 inches from the filament. This water-cooled electron gun is located directly above the specimen disk and is controlled by a power supply. The filament is constructed from two 0.023-inch molybdenum wires, 2 inches in length and interwound. The evaporating material used is a 3-inch-long, 0.020-inch-diameter gold wire of 99.999-percent purity. This gold wire is wound around the molybdenum filament, which is inserted in the filament holders. Disk specimen temperature is measured by two Chromel-Alumel thermocouples placed inside the specimen holder and is then recorded by a temperature recorder.

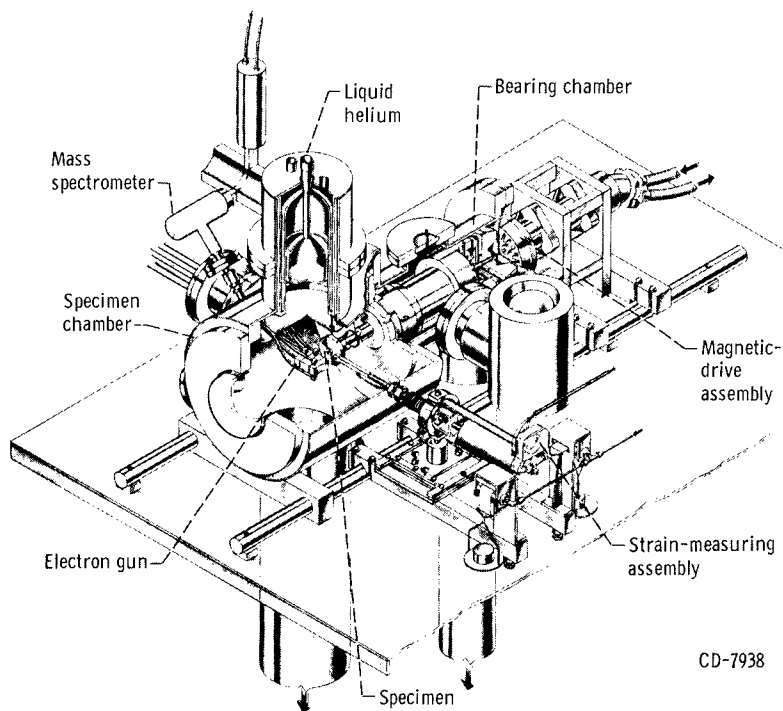
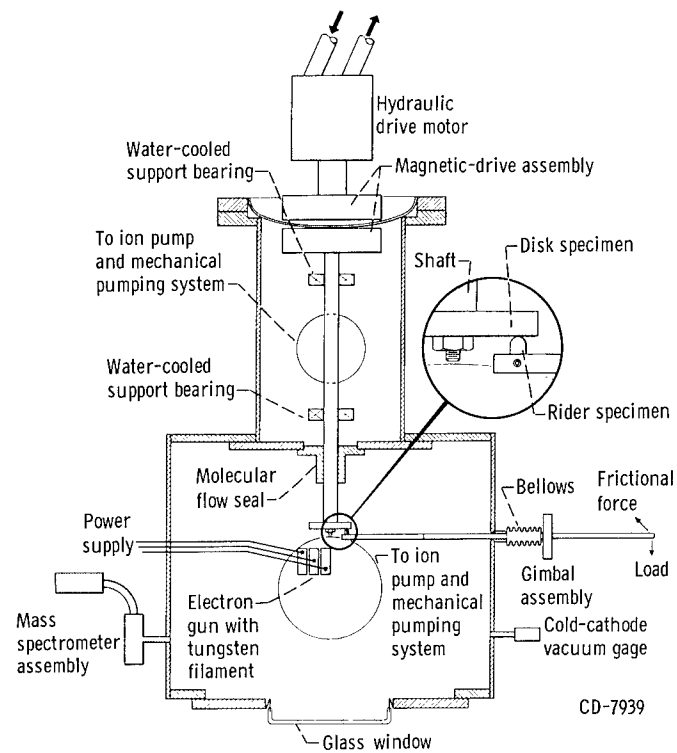


Figure 2. - Ultra-high-vacuum friction apparatus.

Before vapor deposition, a movable shield is placed in front of the substrate so that both filament and gold can be well degassed before any material is deposited on the substrate.

In addition to the mechanical pump, the three-stage oil diffusion pump, and the liquid-nitrogen baffle that are part of the vacuum system, two other pumping systems were introduced: (1) a stainless steel dome which was placed just below the top of the bell jar and functioned as a cryopump while being cooled by liquid nitrogen and liquid helium, and (2) a liquid-nitrogen-cooled titanium sublimation pump. The pressure was measured with a nude, hot-cathode ionization gage, and the vacuum was approximately  $10^{-8}$  millimeter of mercury.

## Ultra-High-Vacuum Friction Apparatus

The vacuum-friction apparatus (fig. 2) was used for determining the coefficient of friction for the coated and uncoated surfaces. The apparatus has two distinct chambers, the specimen chamber and the bearing chamber, both of which are connected to the fore-pumping system.

The forepumping system of the apparatus consists of a cold trap, which is made up of molecular sieves backed by liquid-nitrogen-cooled containers. This system is connected to two mechanical pumps through a 2-inch stainless steel vacuum valve.

The specimen chamber, which is connected to the mechanical pumping system by a bakable high-vacuum valve, is provided with a 400-liter-per-second ion pump, as well as cryopumping surfaces (liquid nitrogen and liquid helium). The specimen chamber contains a cold-cathode (Kreisman) vacuum gage for measuring pressures. The pressure in the specimen chamber is approximately  $10^{-11}$  millimeter of mercury. The specimen and bearing chambers are bakable at  $700^{\circ}$  and  $400^{\circ}$  F, respectively.

The bearing chamber, which is connected to the forepumping system by a 2-inch valve, is equipped with a 125-liter-per-second ion pump, which is placed in operation only after the mechanical pumping system has reduced the chamber pressure to about  $10^{-4}$  millimeter of mercury. The bearing chamber also contains a liquid-nitrogen-cooled titanium sublimation pump. This pumping mechanism is used to pump the bearing chamber to about  $10^{-10}$  millimeter of mercury in preparation for an experiment.

The rotating shaft, upon which the  $2\frac{1}{2}$ -inch disk specimen is mounted, is supported on bearings in the bearing chamber. The shaft support bearings have a large clearance and are mounted in a cartridge so that the shaft expansion takes place into the test chamber and the possibility of the magnet striking the diaphragm is eliminated. Since loading was applied by deadweights, the expansion did not change the load on the specimens. The bearing cartridge is water cooled to prevent any damage to the bearings during the bake-out cycle.

The rotating shaft projects through the rear wall of the test chamber first and then through a molecular flow seal (fig. 2). On the bearing-chamber end of the shaft is mounted a 20-pole magnet, which is separated from a similar magnet, outside the vacuum chamber, by a 0.030-inch diaphragm (0.160-in. air gap). The drive magnet, outside the chamber, is powered by a hydraulic motor with a variable speed capability of 4000 rpm (sliding velocity, 2000 ft/min). Because of instabilities in the drive motor at low speeds (10, 20, and 100 rpm), these speeds were obtained by utilizing a speed reducer with a ratio of 10.

The disk specimen is mounted on the end of the horizontal shaft in the test chamber. Against the disk, a 3/16-inch hemispherical rider specimen is loaded. The rider is held in place by a rigid arm, which projects through a port in the side of the vacuum chamber. The seal (0.030-in. gold O-rings) is made at the wall by utilizing a bellows connection between the chamber wall and the rigid arm. A removable gimbal assembly, which is used to load the rider against the disk surface and to monitor the frictional force through a strain-gage assembly, is fastened to the rigid arm outside the vacuum chamber.

## PROCEDURE

### Specimen Preparation and Mechanical Polishing of Surfaces

The nickel disks used in this investigation were prepared from electrolytic nickel. Small nickel slugs were placed in a zirconium oxide crucible and the crucible was placed in an induction vacuum furnace, which was then evacuated. After evacuation, the furnace was filled with argon and the metal was melted. Once molten, the liquid nickel was poured into a copper mold and cooled to room temperature. The nickel-alloy disks used in this investigation were prepared in a similar manner. Afterward, the castings were machined to the required dimensions. Before the disk specimen was mounted in the high-vacuum evaporation apparatus for electron-bombardment cleaning and vapor deposition, the disk was mechanically ground with 400- and 600-grade emery papers. It was then finished with levigated alumina on a lapping wheel.

Once the surface was micropolished, vacuum deposition was performed at two temperatures on two surfaces: (1) at room temperature on a micropolished surface which had not been cleaned by electron bombardment, and (2) at 800° F, on a micropolished surface which had been cleaned by electron bombardment.

### Thermal Etching

The substrate surface was cleaned under high-vacuum conditions ( $10^{-6}$  to  $10^{-7}$



mm Hg) by electron bombardment. During bombardment, the disk was kept at ground potential and served as the anode; the electrons were supplied by an annular tungsten cathode, which was kept at applied voltages of 3.5 to 4.5 kilovolts and a beam current of 70 to 80 milliamperes. The electron-bombardment cleaning was performed for approximately 30 to 45 minutes, and the disk temperature was in the range 1100° to 1200° F. Electron bombardment can be used for both cleaning the surface and heating the substrate material, if the electron beam is kept on continuously.

During electron bombardment (ref. 4), the surface is cleaned by dissociation of the contaminants (i.e., adsorbed gases or oxides). Considerable energy is then liberated, the substrate temperature is increased, and surface topography is changed. This thermal process, known as thermal etching (refs. 7 and 8), develops grooves where the grain boundaries intersect the surface and produces selective etching on the faces of individual grains. This selective-etching effect occurs because different planes and grain boundaries have different surface energies (ref. 9). Grain boundaries have a relatively high surface energy with respect to the crystals and are, therefore, the preferential sites for thermal etching and solid-state reactions (ref. 7). It is believed (ref. 9) that evaporation (either of metal or of oxide) appears to be the dominant mechanism in the formation of the etched structure.

## Vapor Deposition

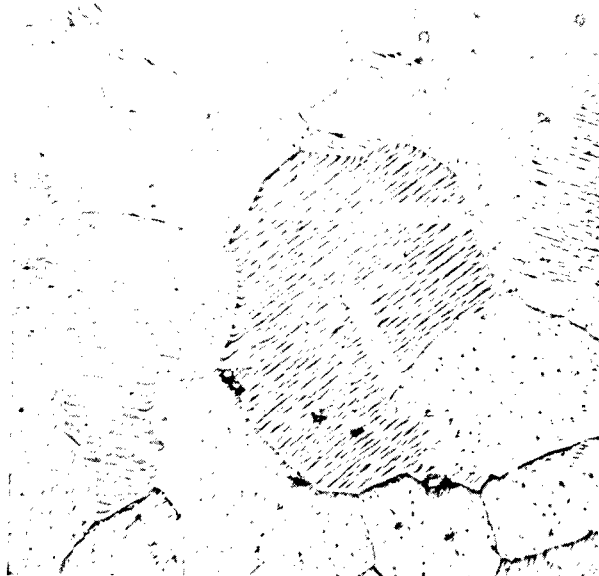
After thermal etching, the electron-beam intensity was gradually reduced, and thus the temperature of the disk was lowered. Once a temperature of 800° F was reached, the electron beam was cut off, and the disk was inverted for vapor deposition of gold. The rate of evaporation depends on the filament current. A current of 35 to 40 amperes was passed through the filament until the temperature was high enough to melt the gold wire and thus wet the molybdenum filament. Once this was achieved, evaporation was allowed for 2 minutes. The thickness of the films deposited was kept at approximately 1800 Å. After deposition, film thickness was measured with an interference microscope.

## RESULTS AND DISCUSSION

The strength and the durability of thin films are determined largely by the degree of adhesion. Adhesion of a vapor-deposited metal film to a metal substrate depends on the formation of an alloyed surface. Very weak adhesion between the film and the substrate occurs when the substrate surfaces are not properly cleaned. The gold films deposited on the "uncleaned" surfaces of nickel, nickel-chromium, and nickel-rhenium disks were



(a) 3-Minute bombardment at 1200° F. X250.



(b) 3-Minute bombardment at 1200° F. X500.



(c) 20-Minute bombardment at 1450° F. X250.

Figure 3. - Copper disks electron-bombarded in high vacuum.  
(Reduced 30 percent in printing.)

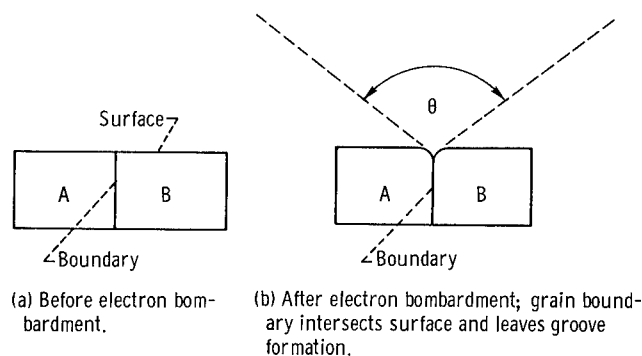
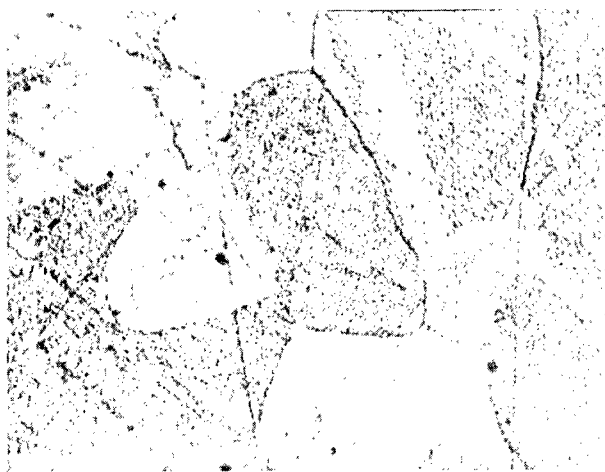


Figure 4. - Thermal etching of grains A and B by electron bombardment.

poorly adherent, as was shown by the scotch tape test and by the friction test. In the first test, if adhesion was poor, the film adhered to the tape rather than to the substrate. This test, although qualitative, gave a good comparison between films with good and poor adhesion. The friction curves for gold films on the uncleaned surfaces (fig. 6, p. 10) show that the coefficient of friction is high and erratic. This indicates a very weak adhesion of gold film to uncleaned surfaces.

Figure 3 shows typical thermally etched copper surfaces. Since copper etches readily in vacuum during electron bombardment, it is a particularly suitable metal with which to illustrate the general phenomenon of thermal etching. If figures 3(a) and (c) are compared, it can be seen that, when the intensity and the duration of the electron beam bombardment are increased, thermal etching will occur particularly at the grain boundaries. A micrograph of figure 3(b) was taken at a higher magnification to illustrate the thermal faceting on the various grains.

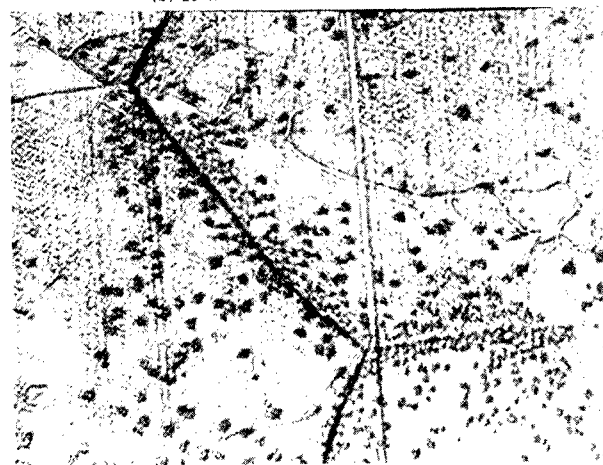
The groove formation at the grain boundaries is illustrated in figure 4. The groove formed can be measured interferometrically (refs. 10 and 11) by the boundary groove angle  $\theta$ . The angle  $\theta$  depends not only on



(a) 5-Minute bombardment at 1150° F.



(b) 10-Minute bombardment at 1100° F.



(c) Gold deposition on substrate after bombardment.

Figure 5. - Electron-bombarded nickel - 10-percent-chromium alloy. X625. (Reduced 15 percent in printing.)

the temperature and time of thermal etching, but also on the orientation of the planes at the particular grain boundary. Since it is believed that evaporation (either of metal or of oxide) is the dominant mechanism for the formation of the etched surface in vacuum (ref. 9), surface cleaning must take place at the same time. Figures 5(a) and (b) show etched surfaces of a nickel - 10-percent-chromium alloy disk which was etched for 5 and 10 minutes, respectively. As the time was increased, the etching became more selective at the grain boundaries.

Micrographs were taken after vapor deposition of gold on the thermally etched nickel - 10-percent-chromium alloy surface (fig. 5(c)). The preferential accumulation of gold in and around the grain boundaries which is indicated can be attributed to the fact that, during vapor deposition, the impinging gold atoms with kinetic energy migrate on the surface and accumulate in the grooves of the grain boundaries (ref. 12). Another factor is the elevated temperature of the substrate during vapor deposition (800° F), which enhances the surface migration of the impinging atoms. This phenomenon indicates that grain boundaries may act as trapping sites and become saturated with deposited atoms.

Since nickel and gold are mutually soluble (ref. 13) and deposition is performed at elevated temperatures, diffusion takes place. It is believed that the strong bonding found between the substrate and the film on the electron-bombarded surfaces is due to the cleanliness of the surface and to the formation of a diffusion type of interface. The diffusion-type interface is characterized by

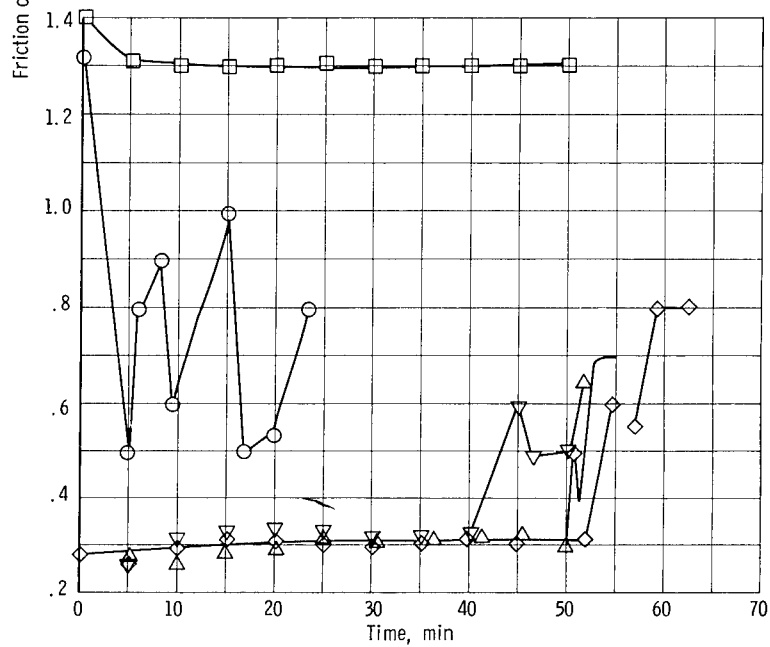
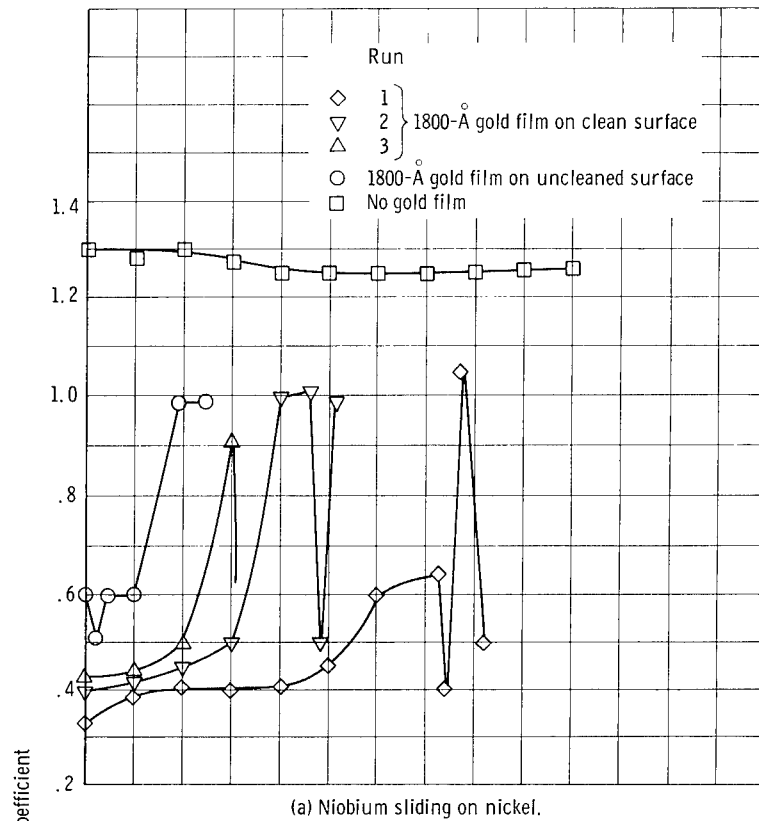


Figure 6. - Friction coefficient of niobium sliding on nickel and nickel alloys, with and without gold film, in vacuum ( $10^{-11}$  mm Hg). Load, 250 grams; speed, 5 feet per minute; temperature, ambient.

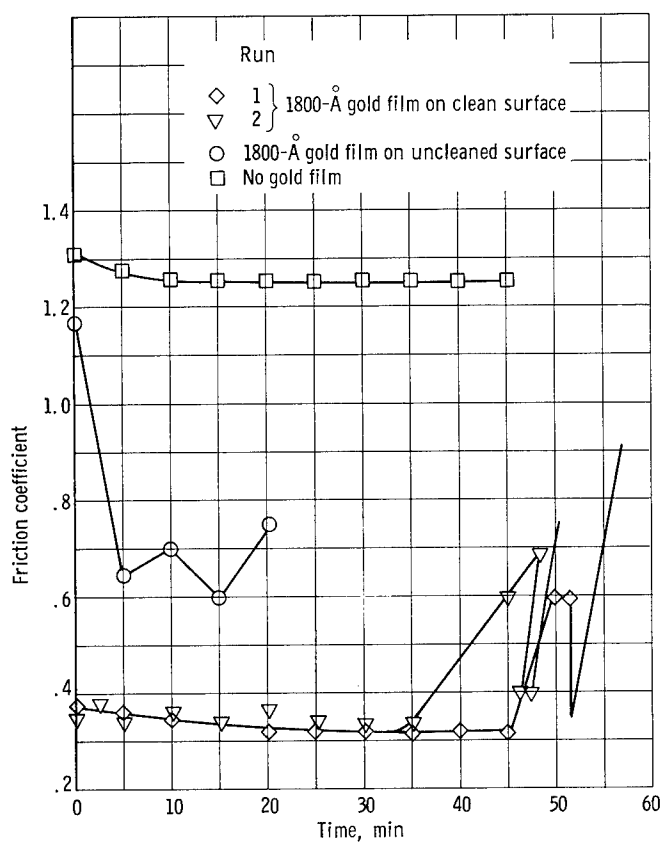
a gradual change in composition across the interfacial region (ref. 6) rather than by a sharp boundary between the film and the substrate.

Intimate contact between the film and the substrate is essential for this diffusion bonding. However, a vacuum-deposited film is in a perfect contact with the substrate. The diffusion rate of gold is not uniform over the entire etched surface. At the grain boundary, the average distance between the atoms is somewhat larger than in the perfect crystal, and therefore a disregistry is formed at the grain boundaries. Because of the presumably "open structure" of the grain boundaries, the rate of diffusion is higher there than it is through crystals (ref. 14). Considering the preferential etching of grain boundaries, the preferential saturation around the grain boundaries of the impinging atoms, and the higher rate of diffusion through the grain boundaries, it can be said that grain boundaries act as "reservoirs" for the deposited material and thus prevent contact of bare metal with bare metal during lubrication.

Very few quantitative studies of the effects of solute on grain boundary diffusion have been done. Some qualitative results have been published in the literature (ref. 15). An investigation had been conducted with silver diffusing into polycrystalline copper alloys. It was observed that the alloying elements in copper had decisive effects on the rate of

silver diffusion along the grain boundaries. According to this investigation, a faster rate of silver diffusion was observed along the copper-alloy grain boundaries.

An electron-beam microprobe study was performed on the gold-nickel specimens of this investigation to differentiate between diffusion in the grain boundaries and diffusion in the grains. By the use of the absorbed electron method, one grain boundary, in one instance, appeared to have a higher gold concentration than the adjacent matrix. Further attempts on other grain boundaries, however, failed to show such an effect. The difficulties are probably the same as those that beset other methods: large beam width, which activates a relatively large area and gives inadequate resolution; and interference from other elements in the specimen, which presents standardization problems.



(c) Niobium sliding on nickel - 5-percent-rhenium alloy.

Figure 6. - Concluded.

The friction curves for gold film on pure nickel (fig. 6(a)) indicate that the film had relatively short durability. The coefficient of friction did not remain at a constant low value but steadily rose to higher values. This continuous rise of the coefficient of friction revealed that pure nickel was a poor friction material and that not even the gold film on a clean surface could afford protection.

The nickel-chromium and nickel-rhenium substrates with gold films (figs. 6(b) and (c)) maintained a coefficient of friction between 0.3 and 0.4 for a relatively long time (45 min). Figures 6(b) and (c) indicate that the films on nickel-alloy substrates had a longer durability during the friction test. This might be attributed to the fact that nickel alloys have higher hardnesses (Brinell 98 to 103) than does pure nickel (Brinell 75).

As the film was broken, the coefficient of friction did not abruptly rise to the value for the bare metal but gradually increased and became erratic. The absence of abrupt change may be attributed to the depth of diffusion and the grain boundary reservoirs, which supply additional lubricant during the friction test.

## SUMMARY OF RESULTS

The following results were obtained from an investigation of vapor-deposited thin gold films as lubricants on nickel and nickel-alloy substrates in vacuum:

1. Marked improvement in film endurance life during friction experiments was obtained with 1880-Å gold films, when substrates were cleaned by electron bombardment and thermally etched prior to deposition of the gold.

2. Vapor deposition of gold on nickel and nickel alloys at 800° F formed a diffusion type interface, in which there was a mutual solubility of the substrate and the film.

3. Nickel-chromium and nickel-rhenium alloy substrates produced longer film durability in friction studies than did pure nickel substrates, presumably because of increased substrate hardness.

Lewis Research Center,  
National Aeronautics and Space Administration,  
Cleveland, Ohio, July 23, 1965.

## REFERENCES

1. Weaver, C.: Adhesion of Thin Films. Second European Vacuum Symposium, G. Kienel, ed., R.A. Lang Verlag, 1963, pp. 193-199.
2. American Society for Metals: Thin Films. ASM, 1964.

3. Hass, G.: Physics of Thin Films. Vol. 1. Academic Press, Inc., 1963.
4. Holland, L.: Vacuum Deposition of Thin Films. John Wiley & Sons, Inc., 1960.
5. Hume-Rothery, W.: Atomic Theory for Students of Metallurgy. Third ed., Inst. Metals, (London), 1960, p. 361.
6. Mattox, D.M.: Interface Formation and the Adhesion of Deposited Thin Films. Rept. No. SC-R-65-852, Sandia Corp., Jan. 1965.
7. Moore, A.J.W.: Thermal Faceting. Metal Surfaces. Am. Soc. for Metals and Soc. of AIME Seminar, ASM, 1963, pp. 155-198.
8. Inman, M.C.; and Tipler, H.R.: Interfacial Energy and Composition in Metals and Alloys. Met. Rev., vol. 8, no. 30, 1963, pp. 105-166.
9. Hondros, E.D.; and Moore, A.J.W.: Evaporation and Thermal Etching. Acta Met. vol. 8, no. 9, Sept. 1960, pp. 647-653.
10. Moore, A.J.W.: The Influence of Surface Energy on Thermal Etching: Acta Met., vol. 6, no. 4, Apr. 1958, pp. 293-304.
11. Hilliard, J.E.; Cohen, M.; and Averbach, B.L.: Grain-Boundary in Gold-Copper Alloys. Acta Met., vol. 8, no. 1, Jan. 1960, pp. 26-31.
12. Mattox, D.M.: Film Deposition Using Accelerated Ions. Rept. No. SC-DR 281-63, Sandia Corp., Nov. 1963.
13. Hansen, M.: Constitution of Binary Alloys. Second ed., McGraw-Hill Book Co., 1958.
14. McLean, D.: Grain Boundaries in Metals. Clarendon Press (Oxford), 1957.
15. Westbrook, J.H.: Segregation at Grain Boundaries. Met. Rev., vol. 9, no. 36, 1964, pp. 415-471.